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TECHNICAL MEMORANDUM

TO: Kurt Hosman – Cascadia Conservation District
 FR: Jay Pietraszek - Golder
 Bob Anderson – Golder
 DATE: September 28, 2007
 OUR REF: 053-1000.300

RE: Status report of the floodplain storage project at Cottonwood Flats

ATTACHMENTS:

Figure 1-1 – Site Location Overview Map Figures 3-1 to 3-4 – Hydrographs Figures 3-5 to 3-6 – Water Level Gradients Figures 4-1 to 4-3 – Storage Estimates Appendix A. Test Pit Logs Appendix B. Sieve Results

1.0 INTRODUCTION

This memorandum is a project status report for the WRIA 46 Step B Storage Assessment. The Step B Assessment focuses on a floodplain storage project that was implemented on the Entiat River, near the Town of Ardenvoir. The project began in February 2007. To this point the project has consisted of a background study of hydrologic and hydrogeologic conditions on the floodplain. Section 2 of this report details the installation of piezometers that are used to measure groundwater levels. Section 3 details the water level data collected from the piezometers. An estimate of the storage capacity of the floodplain site is provided in Section 4.

This work is being completed under the WRIA 46 Water Storage Assessment under Grant C0500165 between the Washington Department of Ecology (WDOE) and Chelan County Conservation District (CCCD).

1.1 Site Description

The study site is on the southwest side of the Entiat River; approximately ³/₄ mile downstream of the Stormy Creek confluence (see Figure 1). The parcel is owned by the Chelan Douglas Land Trust, and is known as "Cottonwood Flats".

The floodplain is bounded by the Entiat River to the North and East and by Tyee Ridge to the South and West. The project site is undeveloped, except for some gravel roads that were built with nonnative material on the center portion of the site. In places this non-native was built up more than one

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foot above the native floodplain material. These roads may act to direct surface flows during highwater periods

A small topographic high runs parallel to the river in center portion of the floodplain. The land surface slopes gently east from the center portion of the floodplain towards the river and west towards a low-lying area adjacent to Tyee Ridge on the southern end of the floodplain. This low-lying area is of particular interest because it may represent a relict side-channel of the Entiat River.

2.0 PIEZOMETERS

2.1 Installation

Nine piezometers were installed on the project site between February 5th and 8th, 2007. Piezometer locations were chosen to best approximate a grid pattern across the floodplain. The location of each piezometer is shown in Figure 1.

The piezometers were installed using a tracked excavator. Batchelor Excavation, of Entiat, WA, was contracted by Golder to perform the excavations. Nine test pits were dug 8-10 feet deep. The depth of each pit was limited by slumping and sloughing on the side walls. Groundwater levels were typically 4-7 ft below ground surface. Double-walled, perforated high density polyethylene (HDPE) pipe was placed in the pit once the maximum depth of the pit was reached. The test pit was then backfilled around the HDPE pipe. Two-inch, schedule 80 PVC pipe was inserted into the HDPE pipe and a pressure transducer was fixed to the PVC.

Piezometer	Surface Elevation (ft ASL)	Depth of Piezometer (ft)
B1	1,561.6	10.0
B2	1,561.8	10.0
B3	1,563.2	9.0
B4	1,562.2	9.0
B5	1,559.3	9.0
B6	1,562.2	8.5
B7	1,561.9	8.5
B8	1,559.2	7.5
B9	1,560.6	8.5

Piezometer Detail Summary.

TABLE 2-1

Pressure transducers were successfully installed in all nine piezometers. CCCD downloaded the data on a monthly basis. Golder compiled and analyzed the data. In August 2007, Golder contracted Pinnacle Surveying of Chelan, WA to survey the piezometer locations and elevations and install several benchmarks on the site.

2.2 Soil Description

Two discreet soil types were observed in each of the test pits: (1) a relatively fine-grained topsoil, and (2) an underlying coarser-grained alluvium. The topsoil was generally fine sands and silts, while the alluvium consisted of coarse to very coarse gravels. In general, topsoil thickness was greater in the test pits located furthest from the river. For example, at test pits B-5 and B-8 the topsoil was up 3 ft thick while less than 1 foot of topsoil was observed at test pits B-1 and B-3. Test pit logs are included in Appendix A.

A particle-size analysis was performed on selected samples from both the topsoil and underlying alluvium. A summary of the results are provided in Table 2-2. The results illustrate that the topsoil is much finer-grained than the alluvium. Particle size distribution plots are provided in Appendix B.

TABLE 2-2

	Site	D ₁₅	D ₃₀	D ₅₀	D ₆₀	D ₈₅
	B9-A	0.3	0.4	0.7	0.8	6.5
. 7	B3-A	0.2	0.7	6.0	13.0	32.0
Гор	B4-A	0.5	0.6	0.8	1.2	19.0
osoi	B5-A	0.1	0.1	0.1	0.1	0.4
1	B7-A	0.2	0.3	0.4	0.5	0.7
	Average	0.2	0.4	1.6	3.1	11.7
Ą	B3-B	1.1	3.2	15.0	23.0	43.0
vllu	B5-B	1.1	4.0	16.0	22.0	50.0
viu	B7-B	0.8	2.3	9.6	16.0	39.0
m	Average	1.0	3.2	13.5	20.3	44.0

Soil Texture Summary

All values are in millimeters.

3.0 PIEZOMETER DATA

3.1 Water Levels

Figures 3-1 to 3-4 show groundwater elevations at the nine piezometers between February 7th and August 21st, 2007. Water levels were at their lowest from February to early March. On March 10th water levels rose quickly then remained relatively stable until the snowmelt runoff began around May 7th. Water levels peaked on June 5th, and then receded sharply until about June 10th. A more gentle sloping recession was observed beginning about June 10th and August 21, 2007.

Figure 3-1 compares the hydrograph from the USGS Entiat River streamflow gage to the hydrographs from the four piezometers (B1, B3, B6, and B9) that are situated closest to the Entiat River on the project site. The USGS streamflow gage (Entiat River at Ardenvoir) is located about 1/3 mile upstream of the project site. The purpose of Figure 3-1 is to show that the water level fluctuations at these four piezometers mirror the water level fluctuations in the river.

Figures 3-2 to 3-4 show hydrographs from all piezometers. The figures are grouped to illustrate the differences in water level fluctuations as the distance from the river increases. The piezometers

situated furthest from the river show a delayed response relative to the piezometers closest to the river. This delay is most evident in piezometers B5 (Figure 3-3) and B8 (Figure 3-4) during two smaller storm events between March 24th and April 24th.

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3.2 Groundwater Gradients

Gradients were calculated between piezometers in two directions: (1) across the floodplain (perpendicular to the river), and (2) down the floodplain (parallel to the river). Figure 3-5 shows the gradients between various piezometers at selected times during the study period. In general, the gradients parallel to the river (or downstream) are higher than the gradients perpendicular to the river (or cross-stream). In other words, the strongest direction of groundwater flow follows the direction of the river.

Figure 3-6 shows the average downstream gradient and the average cross-stream gradient aver the study period. A positive gradient indicates that groundwater is moving from the floodplain to the river (a river-gaining condition). A negative gradient indicates that groundwater is moving from the river to the floodplain (a river-losing condition). The average cross-stream gradient is positive (gaining) from March to late April, negative (losing) from late April through late July, and neutral during August and September.

4.0 STORAGE CALCULATIONS

Groundwater storage volumes were calculated using the following equation:

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Floodplain area (Acres) * Change in water level (feet) * Specific yield (dimensionless)
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A description of the methodology used to determine each value is provided in the following subsections.

4.1 Floodplain Area

The floodplain area was calculated using standard GIS tools. The boundary of the floodplain used in the calculation is shown in Figure 1-1. The floodplain area is 16.61 acres.

4.2 Change in Groundwater Level

The change in groundwater level is the difference between the annual minimum groundwater elevations and either the maximum groundwater elevation or the ground surface elevation. The ground surface elevation was used for the six piezometers which recorded maximum water levels above ground surface. Surface water storage is treated as a separate component of the floodplain's storage capacity and is discussed further in Section 4.5.

The average change in groundwater elevations based on the difference between the annual minimum and maximum, is 3.3 feet.

4.3 Specific Yield

Specific yield (SY) is a ratio of the amount of water that is available to drain from a volume of material to the total volume of material. A range of specific yield values from 0.1 to 0.2 were used

for the storage calculations. This range is consistent with published values for sands and gravels (Fetter, 1994).

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4.4 Groundwater Storage estimates

Using the values discussed above the range of maximum groundwater storage capacities is:

- 16.61 Acres * 3.3 feet * 0.2 SY = **11.0 Ac-ft**
- 16.61 Acres * 3.3 feet * 0.1 SY = **5.5 Ac-ft**

Maximum storage on the floodplain was reached when water elevations peaked on June 5th. Storage volumes declined as water levels receded through the summer, as shown on Figure 4-1. Zero storage was reached when water levels receded to their pre-runoff levels on August 20th.

As shown on Figure 4-1, the floodplain loses water to the river at a rate of about 5 AF per month (0.08 cfs).

4.5 Surface Water Storage estimates

As discussed above, water elevations rose above ground surface at six (B1, B2, B4, B5, B8, and B9) of the nine piezometers. Accurate determination of the surface water storage on the floodplain is difficult because the total area of the floodplain that was underwater, of inundated, was not measured. The transducer data indicate that most of the standing water occurred on the western half of the floodplain, and the average maximum depth of surface water was about 2 feet.

A rough estimate is to assume half of the floodplain (8.3 acres) was inundated during peak runoff and the average depth of the surface water was 2 feet. This nets a surface water storage estimate of 16.6 acre-feet.

Surface water levels across most of the floodplain dropped below ground surface within a few days after water levels peaked on June 5th. Only piezometers B5 and B8, which are situated in the low-lying area on the far west side of the floodplain, had standing water after June 12th. This low-lying portion of the floodplain encompasses approximately 5 acres.

4.6 Potential for Increasing Floodplain Storage

There is potential to increase floodplain storage on the project site. The "storage" would be achieved by reducing the rate that the floodplain discharges back to the river. By keeping this water in the floodplain longer, flows in the Entiat River should increase relative to current conditions during the late summer.

Figure 4-2 shows the current seasonal decline in storage volumes on the floodplain compared to a hypothetical "post-storage" condition. In the hypothetical condition, the seasonal decline in storage volumes is reduced by 50%, to approximately 2.5 AF per month. By slowing the rate of decline, groundwater discharge back to the river is reduced, but the total duration is lengthened and discharge to the river in the late summer is increased.

In order to reduce the rate of floodplain discharge back to the river during the summer, we think it would be possible to construct a relatively small pond in the low-lying area on the southwest side of

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the floodplain, near piezometer B-9. The pond would increase groundwater heads and reduce the gradient of groundwater flow to the river in this area. It is possible that the pond could also be larger in size and encompass the entire back channel area, extending toward piezometers B-5 and B-8. Figure 4-3 shows the conceptual lay-out of the floodplain channel. The outlet for the pond would require some engineering design to determine the elevation and outlet flow capacity. The design would also allow varying levels of control over the water surface elevations in the pond.

Specific details about the design and implementation of this type of project would be finalized in subsequent phase of work.

FIGURES



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APPENDIX A

TEST PIT LOGS

Test Pit: B1Location: Entiat FloodplainDate Installed: 5 Feb 07 15:31Engineer: PietraszekContractor: Batchelor Excavation

INSTALLATION NOTES

Depth (ft bgs)	Description		Sam	ples
	Brown (f-m) SAND, sm silt, sm organic material, It-	No		Depth
0-2.5	sm cobbles, lt-tr clay. (Topsoil)	1		5
2 5-6	Brown speckled (c) GRAVEL and COBBLES, It-sm	2		10
2.5-0	Same as above but with $sm(m_c)$ sand and t_cm silt			
6-10	(Alluvium)			Depth of Hole
		Tin	ne	(ft bgs)
Special Notes:		15:	30	0
Hit water at 2.5	feet. Very coarse material intersected at 2.5 feet.	16:	00	10
Material became slightly finer at about 6 feet.		16:	30	0









Test Pit: B2Location: Entiat Floodplain_Date Installed: 5 Feb 07 14:30Engineer: PietraszekContractor: Batchelor Excavation_

INSTALLATION NOTES

Depth (ft bgs)	Description		Sam	ples
	Brown (f-m) SILT, sm sand, sm organic material, It-	No		Depth
0-2	sm gravel. (Topsoil)			None
	Brownish-black (f-c) Sand and GRAVEL, sm silt,			
2-5	loose (Medium Alluvium)			
	Gray (f-c) SAND and GRAVEL, sm cobbles, tr wood			Danth
5-10	(m-c Alluvium)			Depth
		Ti	ne	(ft bgs)
Special Notes:		14	:30	0
Hole began cavi	ng at about 6 feet bgs	14	:50	10
Water at 5 feet b	bgs	15	:15	0



Test Pit: B3Location: Entiat FloodplainDate Installed: 6 Feb 07 15:20Engineer: PietraszekContractor: Batchelor Excavation

INSTALLATION NOTES

Depth (ft bgs)	Description	S	amples
0-0.5	Brown (f-m) Topsoil	No	Depth (ft)
	Light brown (c) SAND and (f-c) GRAVEL, sm	1	0-1
	cobbles, loose, dry, weakly stratified (Coarse	2	8
0.5-1	Alluvium)		
1-2	(m-c) SAND, sm gravel		Depth
2-9	SAME AS 0.5-1 (Coarse Alluvium)		of Hole
		Time	e (ft bgs)
Special Nataou V	Notor appointered 6 E feet has	15:30	0 C
	valer encountered 6.5 reet bgs	15:4	5 9
		16:0	0 0



Test Pit: <u>B4</u>Location: <u>Entiat Floodplain</u>Date Installed: <u>6 Feb 07 13:13</u>Engineer: <u>Pietraszek</u>Contractor: <u>Batchelor Excavation</u>

INSTALLATION NOTES

Depth (ft bgs)	Description] [
	Medium brown (f-c) SILT and (f) SAND, sm organic		
0-1.5	material, little stiff (Topsoil)		
	Brown (m-c) SAND, It-sm (f-c) gravel, It-tr cobbles,	1	
1.5-7	weakly stratified		
	Grayish-brown (c) SAND and (f-c) GRAVEL, sm		
7-9	cobbles (Coarse Alluvium)		

Samples		
No	Depth (ft)	
1	1.5-3	
2	8-9	

Time	Depth of Hole (ft bgs)
13:15	0
13:50	9
14:05	0

Special Notes: Hit water at 6-7 feet bgs



Test Pit: <u>B5</u>Location: <u>Entiat Floodplain</u>Date Installed: <u>6 Feb 07 14:30</u>Engineer: <u>Pietraszek</u>Contractor: <u>Batchelor Excavation</u>

INSTALLATION NOTES

Depth (ft bgs)	Description	
	Dark brown (f-c) SILT sm organic material,	
0-1	moderately stiff (Topsoil)	
1-3	Medium brown (f-c) SILT It (f) sand, moderately stiff	
3-7	Gray (f) SAND, sm silt	
	Grayish-brown (c) SAND and (f-c) GRAVEL, sm	
7-9	cobbles (Coarse Alluvium)	

Samples		
No	Depth (ft)	
1	0-1	
2	8-9	

Time	Depth of Hole (ft bgs)
14:30	0
14:45	9
15:00	0

Special Notes: Hit water at 7 feet bgs



Test Pit: <u>B6</u>Location: <u>Entiat Floodplain</u>Date Installed: <u>6 Feb 07 08:30</u>Engineer: <u>Pietraszek</u>Contractor: <u>Batchelor Excavation</u>Project: <u>053-1000.300</u>

INSTALLATION NOTES

Depth (ft bgs)	Description		S	amples
	Dark (m-c) SAND (top-soil), It-sm (f-c) gravel and		No	Depth (ft)
0-2	cobbles, sm organic material, loose		1	0-1
2-4	Brown SAND and GRAVEL, sm cobbles		2	5-7
	Brown (c) SAND and (c) GRAVEL, cm cobbles	רך	_	0.
4-7	(coarse alluvium) slightly coarser than above			
	(m-c) GRAVEL and COBBLES, sm SAND, wet			
7-8.5	(coarse alluvium)			

Special Notes:
Hit water at about 5 feet bgs.
Material appears weakly stratified below 5 feet bos. All material is
loose. Hole begins caving below 6 feet.

Depth of Hole Time (ft bgs) 08:45 0 9:05 8.5 9:25 0



Test Pit:B7Location:Entiat Floodplain_Date Installed:6 Feb 07 10:30Engineer:PietraszekContractor:Batchelor Excavation_Project:053-1000.300

INSTALLATION NOTES

Depth (ft bgs)	Description	
	Brown (f-m) SAND, sm organic material, loose	N
0-1	(topsoil)	1
1-2	Brown (m-c) SAND and (f-c) GRAVEL, sm cobbles	2
	Brown (m-c) SAND, sm (f-c) gravel (slightly finer than	
2-3.5	above)	
	Brown (m-c) SAND and (f-c) GRAVEL, sm cobbles	
3.5-8.5	(loose, clean) (coarse alluvium)	

Special Notes: Water at 5 feet. Weakly stratified below 3 feet.

Samples		
No	Depth (ft)	
1	0-1	
2	8	

Time	Depth of Hole (ft bgs)
10:35	0
10:50	8.5
11:15	0



INSTALLATION NOTES

Depth (ft bgs)	Description	
	Dark Brown SILT, sm organic material, sm (f) sand	
0-3	(little plastic, firm) (topsoil)	
3-3.5	Gray (m-c) sand, loose	
	Brown (m-c) SAND, sm (f-c) gravel, little cobbles	
3.5-7.5	(alluvium)	

Samples		
No	Depth (ft)	
1	0-2	
2	7	

Time	Depth of Hole (ft bgs)
12:00	0
12:15	7.5
12:40	0

Special Notes: Hit water at 5 feet. Hole collapsed below 7.5 feet. Could not excavate below 7.5 feet.



INSTALLATION NOTES

Depth (ft bgs)	Description	
0-1	Brown (f-m) SAND (topsoil)	No
	Light Brown (m-c) SAND, sm (f-c) gravel, tr silt	1
1-4	(loose) (alluvium)	2
	Brown (c) SAND and (f-c) GRAVEL, sm cobbles,	
4-8.5	loose (coarse alluvium)	

Special Notes: Hit water at 4.5 feet. Hole collapsed at 8.5 feet.

Samples		
No	Depth (ft)	
1	1-2	
2	8	

Time	Depth of Hole (ft bgs)
9:45	0
10:15	8.5
10:25	0



APPENDIX B

SIEVE RESULTS















